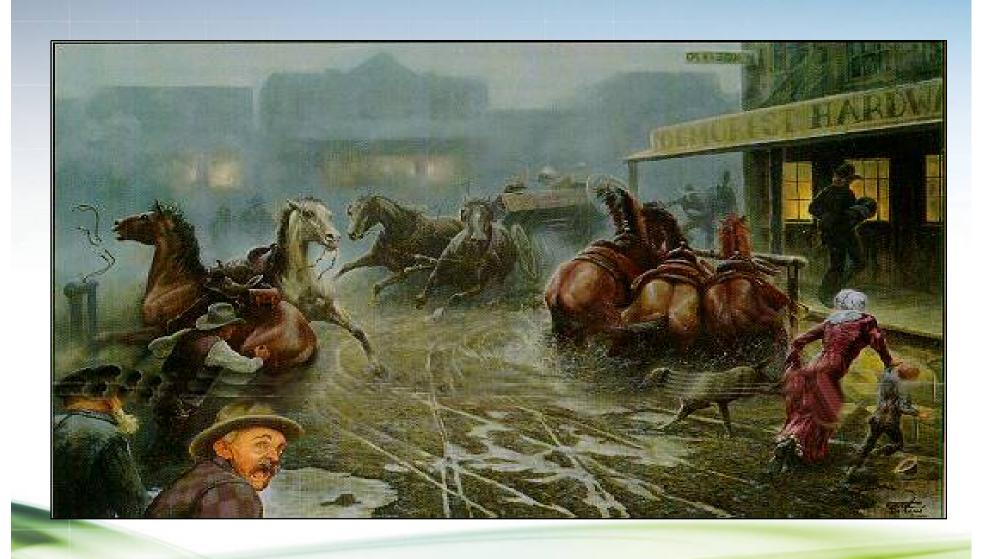
Methods for Effective Room Air Distribution

Dan Int-Hout Chief Engineer, Krueger Richardson, Texas





Where We Are Today:



Agenda

- Overview
- LEED issues and Update
- Perimeter
- Acoustics
- Thermal Comfort
- IAQ / Standard 62.1 Update
- Air System Selection
- Summary



LEED:

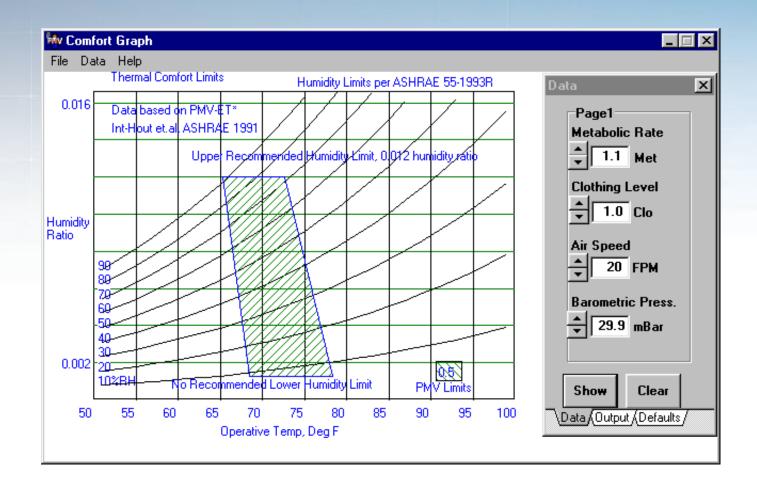
- The challenge from Architects to the Mechanical Engineer is to achieve energy efficiency 30% better than the base systems in ASHRAE 90.1
- The Base System is VAV / Overhead (well mixed).
- As a result, engineers are looking at alternate systems, which include;
 - Underfloor Air Delivery (UFAD)
 - Displacement Ventilation
 - Chilled Ceilings and Beams
- Most Energy Calculation programs, however, have not been validated for systems other than VAV overhead.
- Based on occupant comfort complaints, we still don't understand how to properly apply overhead VAV systems.

Thermal Comfort

Thermal Comfort:

- Latest THERMAL COMFORT STANDARD: ASHRAE 55-2010
- ASHRAE Fundamentals, Chapter 7
- PMV predicted mean vote a single number rating.
- A program is available, based on the new ASHRAE 55-10, which allows plotting of the comfort envelope.
- Standard 55 mandates a maximum 5°F vertical temperature stratification.

Thermal Comfort / Graphical solution



Comfort Economics

ASHRAE Journal, June 2008

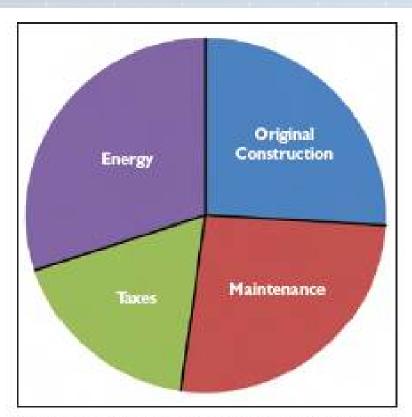


Figure 1: Life-cycle building costs breakdown.

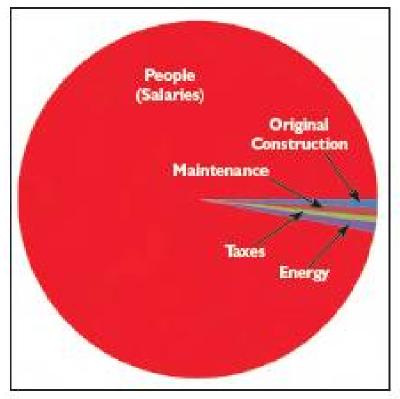


Figure 2: Life-cycle building costs breakdown with people (salaries).

LEED '09 ASHRAE Std 55 Checklist

COMPLETE SECTION TWO FOR PROJECTS USING THE PMV/PPD METHOD SAMPLE COMPLIANCE Weather data used for design calculations Based on Standard 55-Local Discomfort Effects **COMPLETE SEC** Verify that local discomfort effects have been considered and are not likely to exceed Standard 55 Assumptions for pers limits. When local discomfort effects are likely to occur, verify that calculations were performed to demonstrate that local discomfort effects are predicted to result in less than 10% dissatisfied occupants. SECTION ONE Space (i.e., Office, Calculations Not Local Discomfort Effect Likely Performed Radiant Temperature Asymmetry Vertical Air Temperature Difference Floor Surface Temperature Draft Heating M * Operative temperature includes radiant effects. See Standard 55.

Acoustics

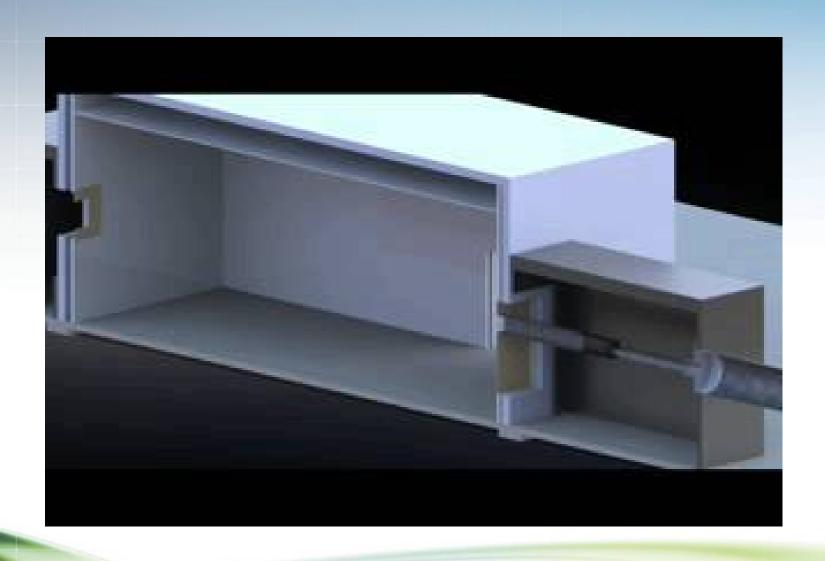
Acoustics:

- AHRI 885-08 acoustical application standard.
- AHRI 880-08 air terminal test standard.
- AHRI 260-01 ducted equipment except air terminals.
- ASHRAE 70, air diffuser performance.
- Acoustical quality suggests the use of RC (or newer measures) rather than NC. Many acousticians are heading back to dBA!
- LEED 2012 will include acoustical credits and requirements.
- A new ruling by AHRI will change everyone's discharge sound ratings considerably.

End Reflection

- Low frequency sound traveling down a duct will partially reflect back when encountering a rapid change in area.
- The smaller the duct, the greater the effect.
- It can be as much as 10dB at 125Hz. It is much less at higher frequencies.
- Since NC is usually set at 125Hz, reported NC can go up as much as 10NC.
- Most importantly, Specifying Engineers should be modifying their discharge sound requirements to reflect the new data.

End Reflection



End Reflection

- An end reflection happens when air travels from a main to a branch duct, and especially when it enters a flex duct connection.
- Another happens when a duct terminates at the room, at the diffuser.
- AHRI 885 includes one 8" end reflection in Appendix E.
- This change only affects reported discharge sound power levels.
- Discharge sound is the same, but will be reported a bit louder.
- Engineers will need to update their discharge sound specifications.

Sound Specifications

- Should be based on clearly stated assumptions.
- Should reflect real project needs, not any manufacturer's data and use currently accepted application factors..
- If duct lining is used require"NC shall be determined in accordance with AHRI 885-08, Appendix E", otherwise specify octave band sound power.
- Specifications need to me modified to account for the new reported data.
- Over-silencing increases both initial costs and operating costs, and may hinder proper IAQ performance.

Indoor Air Quality

Indoor Air Quality

- Standing StandardProject Committee62.1
- •Residential Committee is 62.2
- •Current Standard is 62.1-'10
- One addenda for the '10 version has already been approved



ANSI/ASHRAE Standard 62.1-2007 (Supersedes ANSI/ASHRAE Standard 62.1-2004) Includes ANSI/ASHRAE Addenda listed in Appendix I

ASHRAE STANDARD

Ventilation for Acceptable Indoor Air Quality

See Appendix I for approval dates by the ASHRAE Standards Committee, the ASHRAE Board of Directors, and the American National Standards Institute.

This standard is under continuous maintenance by a Standing Standard Project Committee (SSPC) for which the Standards Committee has established a documented program for regular publication of additinds or revisions, including procedures for timely, documented, consensus action or regulars for change to any part of the standard. The change submittal form, instructions, and deadlines may be obtained in electronic form from the ASHRAE Wide site. High joiness actions or in paper from from the Manager of Standards. The latest edition of an ASHRAE Standard may be purchased from ASHRAE Customer Service, 1791 Tuttle Circle, NE, Afanta, GA 30329-2305. E-mail: orders 8 ashness on p. Fax. 404-537-5478. Telephone: 404-636-8400 (worldwide), or toll free 1-600-527-4723 (for orders in US and Canada).

© Copyright 2007 ASHRAE, Inc.

ISSN 1041-2234



American Society of Heating, Refrigerating and Air-Conditioning Engineers, Inc. 1791 Tulle Circle NE. Atlanta. GA 30329

www.ashrae.o

IAQ Standard

- Standard 62 is on continuous maintenance.
- Continuous and incremental changes are in progress.
- It will attempt to be in coordination with building codes.
- A Guideline document for designing systems above minimum requirements is being created.
- Users Manual is available now.
- The IMC has referenced 62.1 in the 09 release of the mechanical code.
- There seems to be minimal public awareness of the dynamic nature of the Standard.

Methods of Air Distribution

Air Distribution Device Selection Guidelines

- The ASHRAE fundamentals handbook, chapter 20 (Air Distribution), provides guidance on several methods of air distribution.
- Methods include overhead fully mixed, as well as fully stratified and partially mixed systems from below, and even task /ambient personal air delivery systems.
- Described delivery systems include constant and variable volume, UFAD, displacement ventilation and chilled beam systems.
- All have advantages and disadvantages, which must be understood by the design engineer and architect.

Well Mixed Overhead Air Distribution

Air Distribution Device Selection Guidelines

- For overhead well mixed systems, one should select a unit with throw at max, and minimum, flow that meets ADPI guidelines based on diffuser spacing and T50 (throw to 50 fpm).
- Additionally, select for maximum mixing:
 - Noise can be good.
 - Dirt on the ceiling is not bad.
- Air Distribution Effectiveness (ADE) is a new term describing room air mixing, and is a parameter with all delivery methods.

Improperly Selected Overhead Air Distribution

POORLY ADJUSTED / SELECTED DIFFUSER

Effective Overhead Air Distribution

PROPERLY ADJUSTED DIFFUSER



ASHRAE Journal, 2004, on overhead air distribution selection

Design Issues:

- Diffuser Selection
- Perimeter
- Thermal Comfort
- Acoustics
- Ventilation & IAQ

Legal Issues

Protection Against Liability For Poor Diffuser Selection

By Daniel Int-Hout III, Member ASHRAE

he manner of achieving an acceptable Air Diffusion Performance Index (ADPI) has been well understood for more than 20 years. Unfortunately, complaints of discomfort abound. It is not uncommon for building occupants who work in the same space to complain that they are "too hot" and "too cold."

Many unconventional designs and new technologies have discharged at 15% of cooling velocities at discharge temporal been used to correct this apparent problem, including displace-tures of 105°F (41°C), Since the warm jet has too much buoyment vertilation, underfloor pressurized plenum air distribution, occupant task conditioning systems, etc. While all of these strategies assume that conventional everhead air distribution is unable to provide acceptable environments, this appears to be a false premise.

According to data and to technical papers as early as 1976, given a properly selected set of overhead ceiling diffusers, and an HVAC supply system capable of meeting the loads in the space, it is possible to devise a system of either VAV or constant volume air distribution than can respond to variations in localized loads from 20% to 100% of designed maximum loads at a variation in space temperature that most occupants will not notice.1 This same system also will provide a ventilation effectiveness of 100% (all the ventilation air supplied at the celling will be delivered to the occupants). Heating performance

with ceiling located diffusers also is well documented. So why are building occupants complaining they're uncomfortable? The likely culput is improper diffuser selection,2 which can lead to a number of problems. The first is "damping." At low airflows, diffuser velocities may not be high enough to create the "Counda effect" necessary to overcome the negative beoyuncy of the cold air being discharged. This cruses cold air to drop into the space. As a result, it's cold under the diffuser, warm at the midpoint between diffusers, and cold air puddles at the floor creating a vertical stratification in the space. Another problem occurs at very high airflows. Jets collide at the midpoint between diffusers, causing cold airstreams to drop into the space (where it was het certier). The increased induction at the recently cold spot under the diffuser now creates an option; warming that location."

At the perimeter (where closed executive offices often are located) even worse things can happen. In winter, air is being

ancy and too little projection to mis with cold air that will spill down the window, there will be an 8°F to 10°F (4.4°C to 5.6°C) temperature difference between 6 in, and 6 ft (0.1 m and 1.8 m) from the floor in the middle of the room (contrary to the minimem requirements of ASHRAE Standard 55, Therreal Environracrial Conditions for Human Occupancy). In surrener, heat rising

from the window stratifies at the ceiling. Cold oir from the diffuser, which is often set to blow down," stratifies at the floor, in both cases, at 43 in. (1.1 m) above the floor, where the thermostat is located, it is 75°F (24°C').

Problems like these can lead to liability and exposure Here are just a few examples. In a Baltimore conductionary complex with two-story living rooms, the designer supabod air from the colding. Since the air was too hot in cold weather, it stratified at the ceiling, resulting in a tempera-

have of 50°F (10°C) at the ankles and 50°F (27°C) at the head. The condominium owners saed the engineer. The case was eventually settled, but not until ofter the engineer incurred fees and costs for atomeys and exports. A similar problem occurred in a one-story bank in Pennsylvania. This time, the case went to trial and the jury returned a sizeable verdiet against the engineer. The expert witness fees alone exceeded the amount in issue in the lawseit.

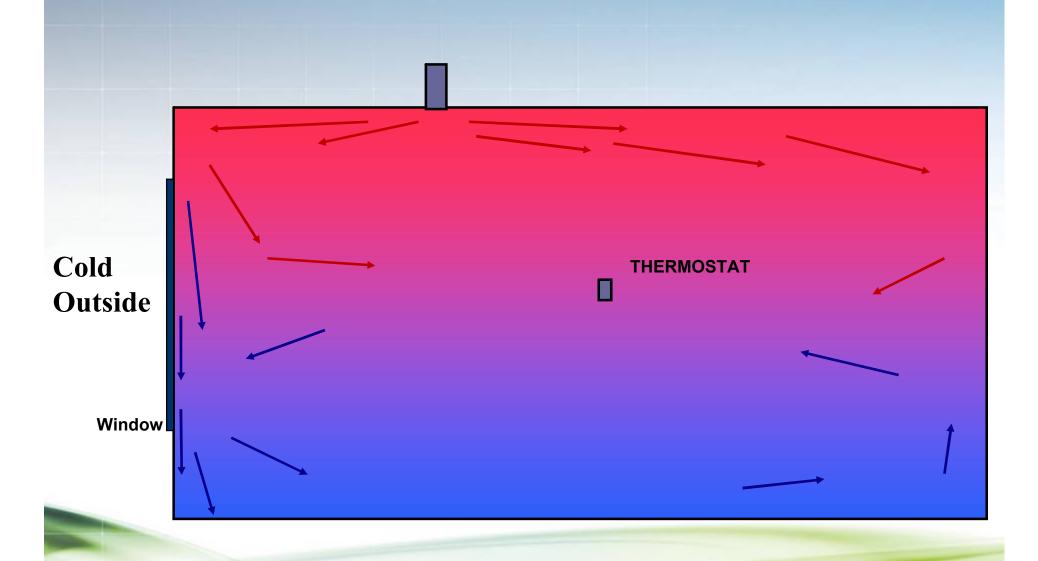
Improper diffuser selection can also lead to problems for owners. For example, in an office building in New Jersey, a tenant successfully broke its lease after complaining about comfort problems relating to criling diffusers. Indeed, according to the Building Owners and Managers Association, thermal comfort related issues (often misdiagnesed as IAO problems) were the No. I reason for non-renewal of leases in 2002.

The information coets/red in this article represents the opinion of the ugher. It is not intended to, and does not, constitute legal advice, redoes it represent the opinion of ASHRAE or any of its bodies.

ashrae.org ASHRAE Journal

September 2004

Common Overhead Heating Design



Overhead Heating Perimeter Considerations:

- Maximum delta-t for effective mixing when heating from overhead, per ASHRAE handbook = ?.
- = 15°F (90°F discharge), continuous operation.
- Throw toward and away from glass.
- 150 FPM should reach 4-5 feet from the floor.
- ASHRAE 62.1 requires that ventilation be increased by 25% when heating, if the above rules are not followed.
- Typical perimeters require only 8°F Delta-t
 @ 1cfm/sq.Ft.

Perimeter Considerations:

See March 2007 ASHRAE Journal:

reprint or port on their web site once the final version has been published. A reprint permission form may

Overhead Heating Revisiting a Lost Art

By Daniel Int-Hout III, P.E., Hember ASHRAE

AV terminals provide a measured quantity of conditioned V air to a space, in response to a control signal from a thermostat or room sensor. This air may be tempered with a reheat. coil, plenum air, or both. The means and selection of parameters for this reheat leads to much of the complexity and questions in selecting and specifying VAV terminals. To avoid problems, selecting the reheat design parameters requires an understanding of the limitations of the reheat coil (hot water or electric) and the means of air distribution.

When these systems were first designed similar, and a consensus recommendaand installed in the late 1970s, several tion was included in the 1979 ASHRAE David ter-Hour St, RE, into chief arguments: manufacturers extensively researched the Handback-Fundamentals. The reconparameters for effective overhead heat- mendation has been in every edition ng. The results of all the research were since. (From the 2005 edition, Chapter

33, p. 33,17: "All researchers found less than optimum performance with high discharge temperatures [greater than 15°F above ambient[.... Under hunting load conditions, the supply air temperause must be limited to avoid excessive thermal stratification." y Unfortunately discussions with design engineers from Missoula, Mont, to San Autonio, and from Los Angeles to Boston reveal that the preparatement of systems is designed for discharge temperatures in excess of 100°F (38°C).

Figure I illustrates a common misapplication. Air is discharged at around 100°F (38°C), and never reaches the cold airstream falling down the window. In this cituation, ventilation air often short

About the Author

* See sko Sonke , D. 30% "Spendard &I. I-3804—Spears Operation: Dynamic Reset Operation * #3HRAE Journal 48(12)34

ASHRAE Journal

March 2007

Overhead well mixed Air Distribution - Pros and Cons

Pros:

- Baseline of 90.1 Energy well documented energy calculation programs
- ADPI can be predicted to validate 55 Vert. stratification
- Well understood construction details
- Heating and cooling commonly accomplished with single system
- Low cost for reconfigured spaces

Cons:

- Difficult (but possible) to guarantee 30% more efficient than 90.1
- Ventilation is shared by all
- System acoustics may be objectionable if not carefully designed
- It's "Old School".

UFAD Underfloor Air Distribution

UFAD: Underfloor Air Distribution

- A raised floor allows electrical and communication circuits to be easily accessed and changed.
- Air may be distributed within this space, without ductwork.

Pressurized plenum for core

Ducted perimeter with fan powered boxes, or other techniques, depending on climate, glass load, etc..

Interior Outlet Selection – 1/workstation



Perimeter outlet selection

- Perimeter solutions vary considerably
- Avoid condensing coils under the floor
- Hydronic coils often leak
- Exhaust at the perimeter to draw heat away
- Best solutions seem to be heat and cool from overhead

UFAD – Pros and Cons

Pros:

- Potential to save energy due to reduced fan static and higher discharge temperatures
- Silent operation, less than 30 NC
- Relatively simple controls needed
- Occupant control of local environment
- Lowest Churn costs with raised floor
- No Validated Energy Modeling programs

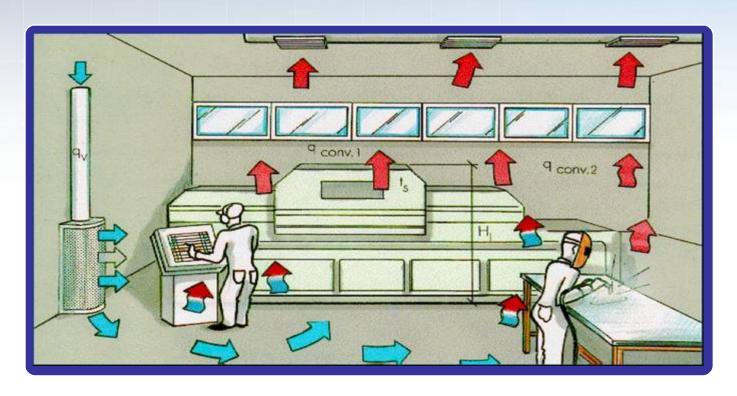
Cons:

- No ASHRAE 55 Vertical Temperature Stratification calculation method (yet!)
- Requires careful building construction to avoid leakage
- Special consideration required in humid climates
- No Validated Energy Modeling programs

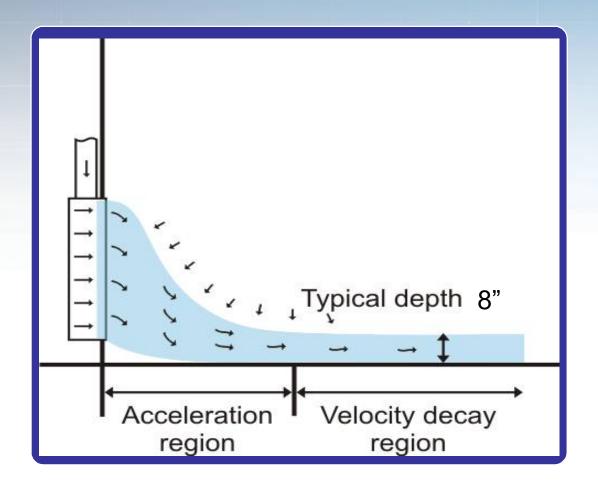
Displacement Ventilation

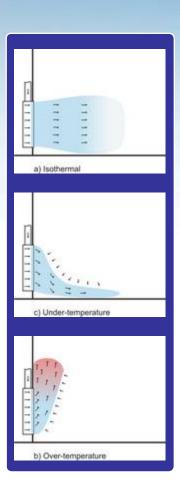
Displacement Ventilation System

 Thermal displacement ventilation is based on cool air supply at low level and stratification of room air temperature and contaminants due to natural buoyancy forces of the heat gains.



Select based on "near zone"





Applications

Classrooms
Kitchen
Restaurant
Auditoriums
Atriums
Gyms
And more...













Displacement Ventilation – Pros and Cons

PROS

- Less cooling energy may be needed
- Longer free-cooling period, depending on climate because of lower discharge temperatures
- Better air quality / reduced outside air requirement
- Quiet excellent for classrooms
- Energy Calculations not validated

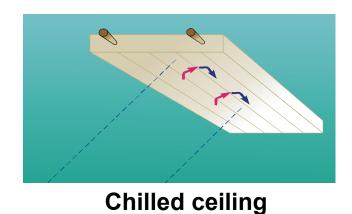
CONS

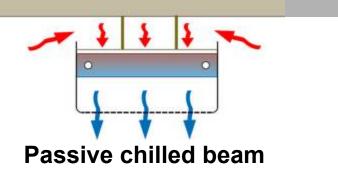
- No advantage if the ceiling height is < 10 ft
- Draft risk near units; velocities should always analyzed
- Enough space for units should be available
- Separate heating system required if exterior walls aren't well insulated
- Must use CFD or other method for vert. Temp. validation.
- Energy Calculations not validated

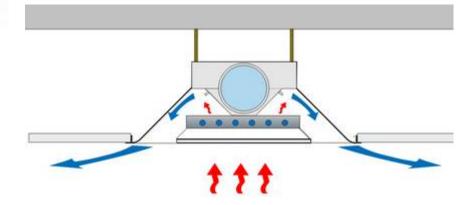


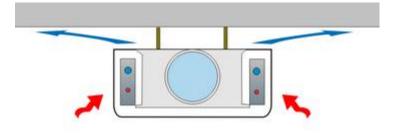
Chilled Beams

Chilled ceiling systems









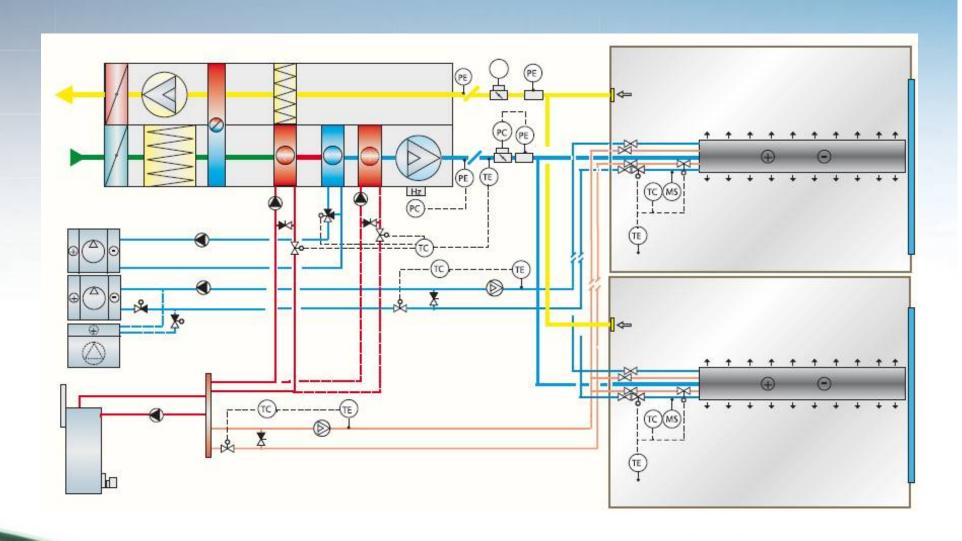
Exposed Active Chilled Beam

Suspended Ceiling Active chilled beam

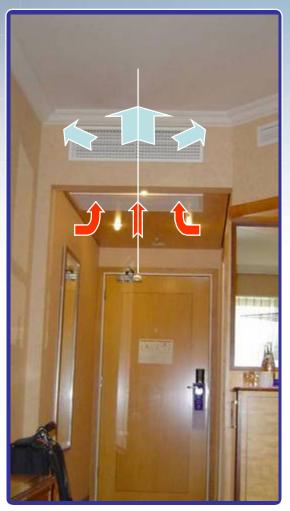
Active Chilled Beams

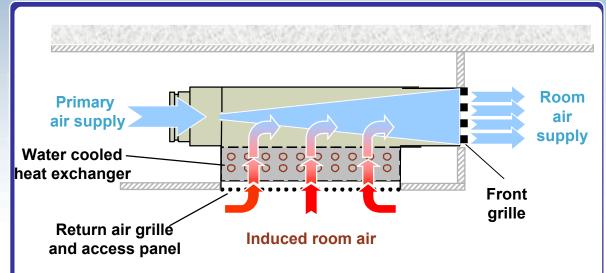
- Remember they are still diffusers
- The same selection rules apply as for other slot diffusers
- Selecting for maximum capacity reduces cost but raises possibility of reheat at part load
- Beams have limited capability in perimeter applications with poor building evnelopes.

Schematic Diagram of a Chilled Beam System



Beams in Hotel Rooms





Chilled Beams – Pros and Cons

Pros:

- Potential to save energy For example: To transfer 1 ton of energy with water consumes much less electricity compared to air.
- Low velocities in occupied space, less than 50 fpm
- Silent operation, less than 30 NC
- Lower units save plenum space, may reduce floor-to-floor height
- Radically smaller ductwork lower fan energy required
- Relatively simple controls needed
- Few (any?) validated energy modeling programs

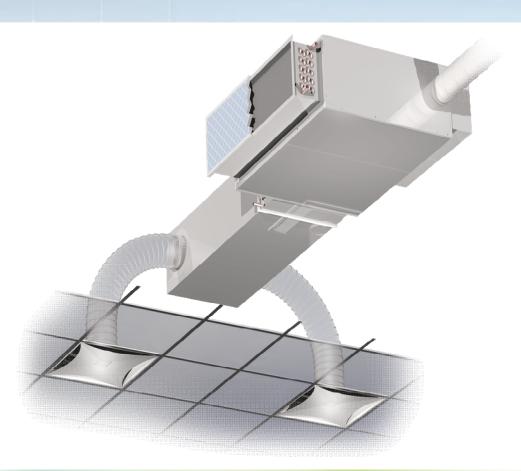
Cons:

- Requires Excellent Building Curtain Wall Construction to control Condensation, especially in humid climates
- High First equipment and installation costs
- No ASHRAE 55 Vertical Temperature Stratification calculation method (yet!)
- Few (any?) validated energy modeling program

Plan B: The Chilled Fan Box Non-condensing Cooling Coil Optional MERV 8 Filter Standard Ceiling Diffuser **Dedicated Outdoor Air Supply**

Chilled Fan Box Summary – Complement to CB

- Increased air distribution flexibility
- Uses same mechanical system as CB
- Complements CB by addressing challenging applications
 - Atria
 - Lobby
 - High humidity locations
 - Higher skin loads
- Minimal Contractor Training
- Guaranteed Performance



Summary

Zero Net Energy Buildings

- ZNEB is a goal that both ASHRAE and the USGBC have set.
- Failure to understand the physics of room air distribution with the different systems now available may, however, result in "ZNAB" – Zero Net Acceptable Buildings.
- We need to understand the pros and cons of the various means available to provide for occupant comfort.

Net Zero Energy Building



Summary

- LEED 2009 (V3) requires meeting Standard 62.1
- ADPI can assure compliance to 55 in the design phase, but only for overhead systems in cooling mode.
- Reheat needs to be carefully considered in terms of discharge temperatures and velocities.
- Acoustics should be specified as maximum allowed octave band sound power.
- DV, UFAD and Beams can supply quiet air in classrooms
- Software is available to assist in selecting the best mix of products.
- Energy Use Calculations of alternate systems needs to be validated.
- The rules are dynamic pay attention.

Contact



dint-hout@krueger-hvac.com

www.krueger-hvac.com